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# SCOPE - Volatile and aerosol-based emissions of aged CESAR1 and their mitigation - measurement and simulation



20/06/2023

The 12<sup>th</sup> Trondheim Conference on CO<sub>2</sub> Capture, Transport and Storage









# SCOPE - Volatile and aerosol-based emissions of aged CESAR1 and their mitigation - measurement and simulation

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## **SCOPE – Sustainable OPEration of post-combustion Capture plants**

Follow the continuous path of the treated gas from source to recipient and ensure a sustainable and environmentally safe operation of the amine-based capture plant



Demonstration of emission management technologies at capture pilot plants

- Validated models to predict volatile and aerosolbased emissions
- Reliable process and operational data, sample analysis, operational and maintenance costs from tests at 6 industrial sites for the assessment of the performance of emission mitigation technologies
- Dependence of emissions on solvents, solvent aging, flue gas properties, plant operation, and capture rate



## SC

Waste-to

Energy

kg CO<sub>2</sub>/

500

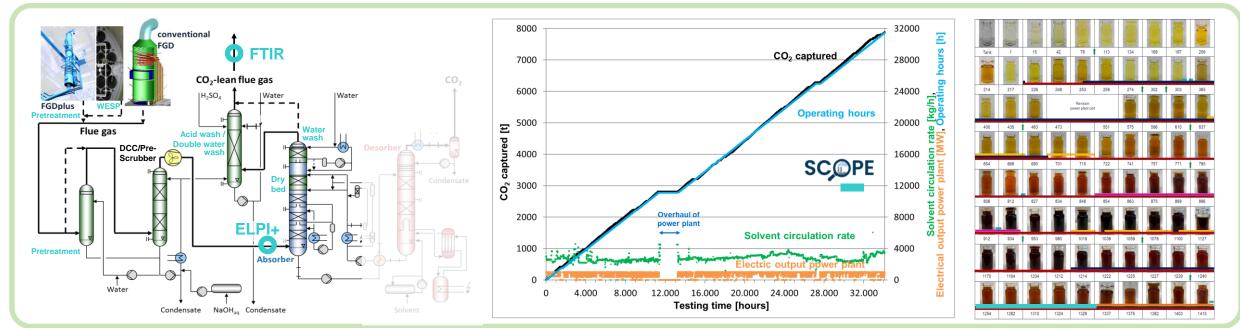
Lignite 300 kg CO<sub>2</sub>/h



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## Test of emission mitigation technologies for CESAR1 at Niederaussem

- Flue gas source: 1,000 MW lignite-fired power plant
- Operation mode: 24/7, 300 kg<sub>co2</sub>/h@90% capture rate, 120-130°C/1.75-2.4 bar(a)
- Solvent: aged CESAR1, aqueous blend of 3.0 M AMP and 1.5 M PZ
- Test of more than **20 configurations of emission mitigation technologies** for **aerosol-based** and **volatile emissions** (water wash, double water wash, acid wash, dry bed (OASE aerozone<sup>®</sup>), pretreatment, WESP)
- Start of measuring campaign: after 29,800 testing hours (1,242 days) without inventory exchange

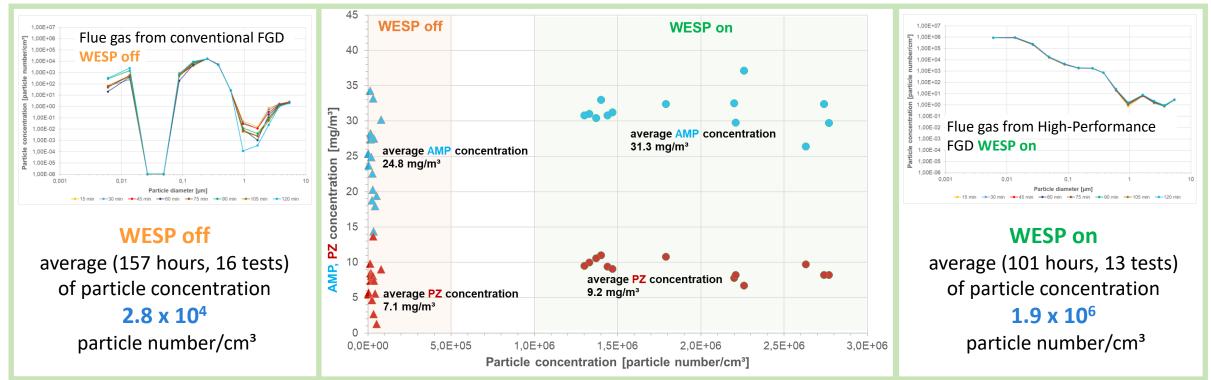




## Generation of aerosol nuclei by the WESP upstream the CO<sub>2</sub> absorber

29 Repeat measurements for the benchmark for emission mitigation: Water wash

- Operating voltage of the WESP (wet electrostatic precipitator) ~35 kV
- Investigation of aerosol-based emissions by ELPI+ (14 size classes, diameter 6-5,400 nm), FTIR (uncertainty ± 3 % relative)
- As expected, the WESP causes increase of the particle number concentration from ~10<sup>4</sup> to ~10<sup>6</sup> particles per cm<sup>3</sup> by the formation of small particles <0.1 μm and increase of the amine emissions >25%

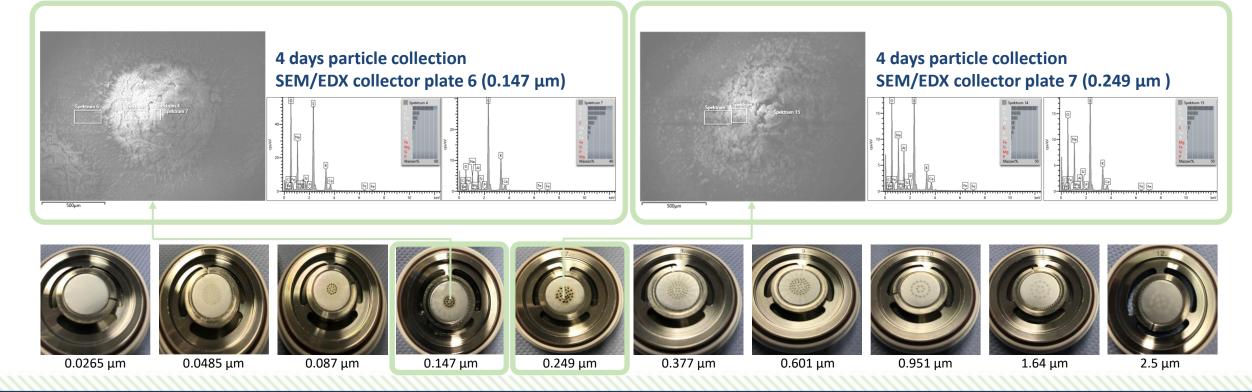




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## Generation of aerosol nuclei by the WESP and their investigation

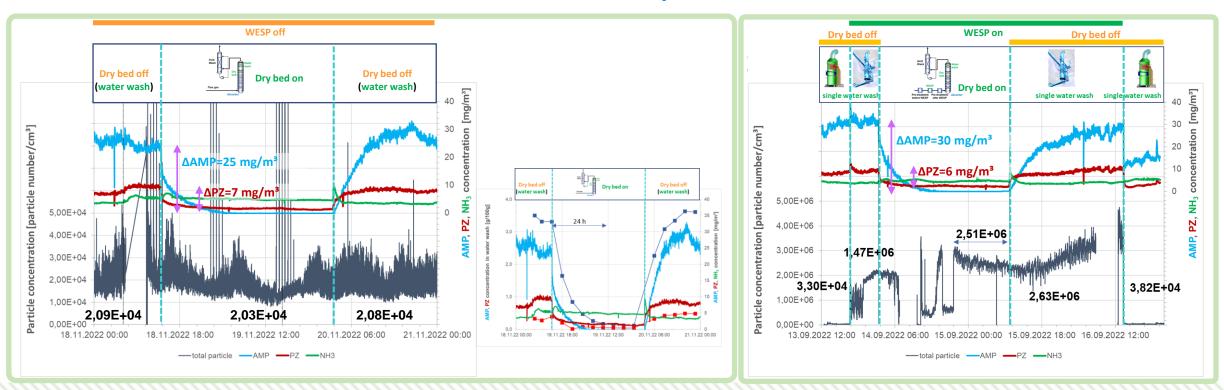
- Macroscopic amounts of aerosol nuclei could be sampled at the inlet of the CO<sub>2</sub> absorber
- Analysis of samples by SEM/EDX
- The solid material consists mainly of Na, S, and O (Na<sub>x</sub>S<sub>y</sub>O<sub>x</sub>, most likely Na<sub>2</sub>SO<sub>4</sub>)
- **Results confirm former analysis** data of single particles



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## Control of volatile and aerosol-based emissions - Example: Dry bed

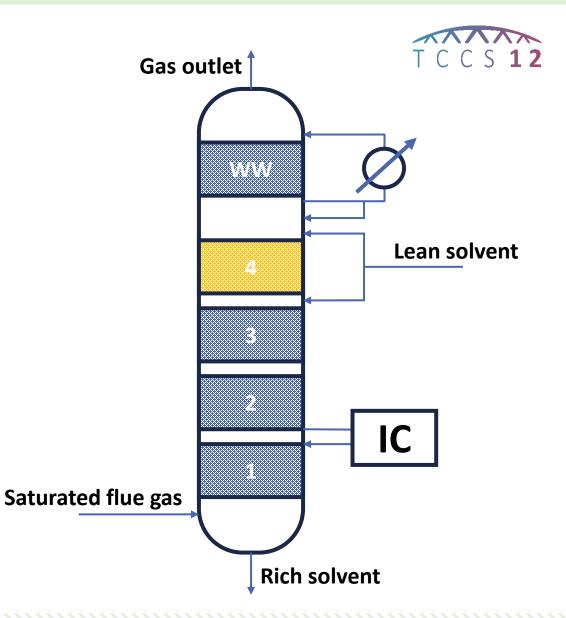
- Strong reduction of volatile and aerosol-based emissions of AMP and PZ by the dry bed
- No effect on emission of NH<sub>3</sub>
- Recommendation: sufficient testing times of 2-4 days for individual tests to be able to evaluate the real effects after the amine concentration in the water wash has achieved steady state



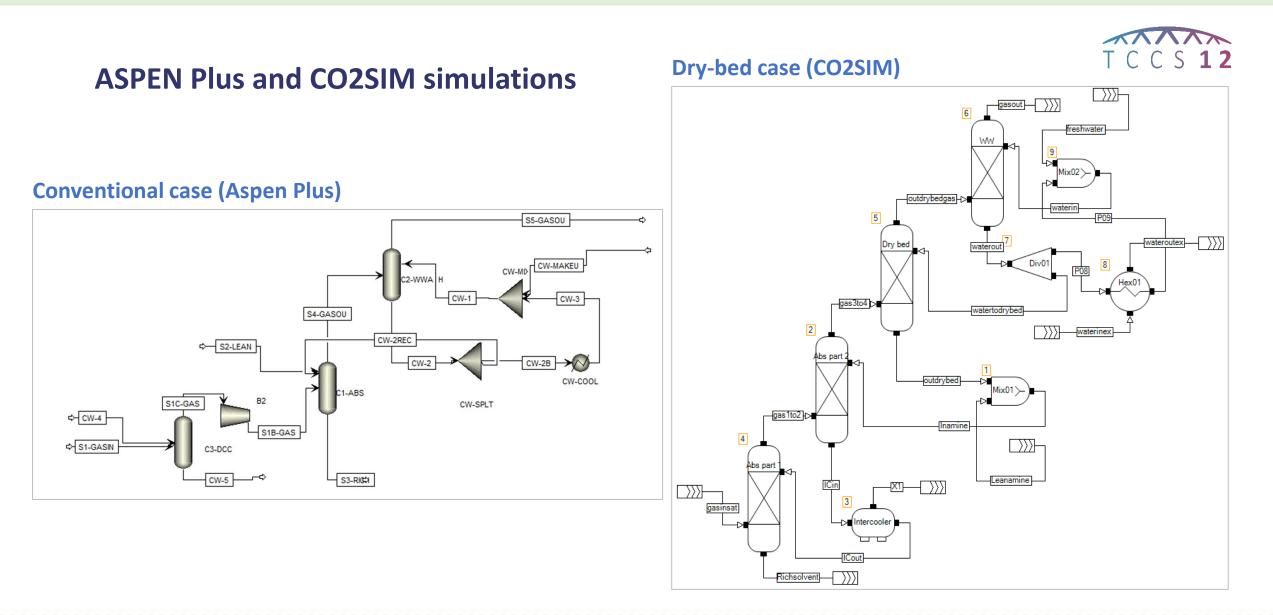


## Simulation of volatile emissions for CESAR1

- 2 cases: with and without dry-bed (conventional)
- 2 software: ASPEN Plus and CO2SIM
- Coal-fired power plant flue gas (15.5% CO<sub>2</sub>) with T<sub>absorber,inlet</sub> ca. 40°C
- 4 packing sections: the 4<sup>th</sup> one can serve as dry-bed if the lean solvent is introduced below it
- 1 water-wash section; a small portion of the water is sent on the top of the 4<sup>th</sup> packing section
- Total intercooler (IC) between the 1<sup>st</sup> and 2<sup>nd</sup> packing section







## SCCPE

## **RWE Experimental test campaign validation**



#### AMP / PZ volatile emissions

• Conventional case

	Wate	er at W/W o	utlet	Flue gas at W/W outlet							
	AMP PZ Total			A	ИР	Р	Z	Total			
	g/100g	g/100g	g/100g	mg/m <sup>3</sup> ppm (mol)		mg/m³	ppm (mol)	mg/m³	ppm (mol)		
RWE (*)	3.38	0.33	3.71	24.90	6.26	8.40	2.19	33.30	8.45		
ASPEN Plus	2.56	0.028	2.59	30.45	9.02	0.007	2.12E-03	30.46	9.02		
RWE	3.50	0.465	3.97	28.42	7.09	8.48	2.21	36.90	9.30		
CO2SIM	-	-	3.52	-	-	-	-	57.10	14.5		

(\*) RWE experimental data with no additional emissions mitigation technologies other than a single water/wash system. Data include aerosol and volatile emissions from a test campaign in which low concentration of aerosol particles were measured

#### • Dry-bed case

	Wat	er at W/W	outlet	Flue gas at W/W outlet							
	AMP	PZ	Total	AMP		PZ		Total			
	g/100g	g/100g	g/100g	mg/m³	ppm (mol)	mg/m³	ppm (mol)	mg/m³	ppm (mol)		
RWE (*)	0.12	0.0435	1,64E-01	ND	ND	1.273	0.33	1.273	0.33		
CO2SIM	-	-	2.41E-01	_	-	-	-	2.64	0.67		



#### **Basic assumptions in the class-based aerosol model**

- Experimental number counts for the various ELPI+ classes used as input
- The particles entering are saturated with Na<sub>2</sub>SO<sub>4</sub>
- A simplified model is developed to calculate the water partial pressure as a function of both Na<sub>2</sub>SO<sub>4</sub> concentration and amine composition.
- No coalescence or break-up of particles.
- The kinetic model for CO<sub>2</sub> absorption into AMP/PPZ blends developed in the ALIGN project is used.

#### Inlet droplet classes and counts

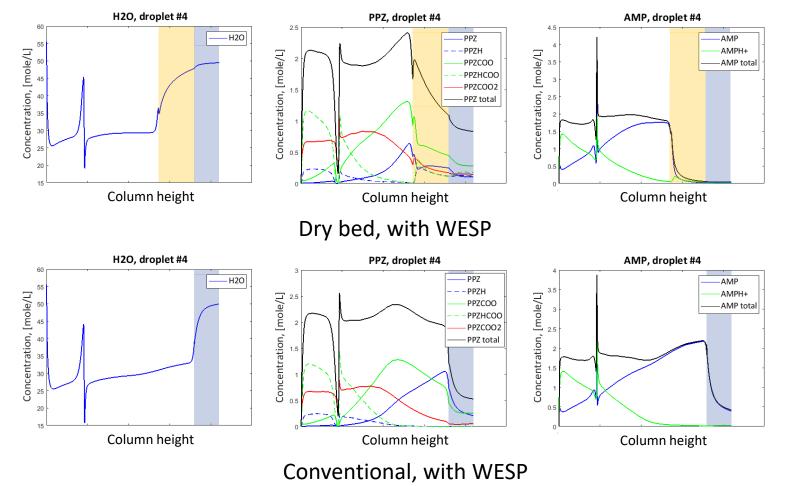
Diameter, nm	6	13.6	26.5	48.5	87	147	249	377	601	955	2500	3700	5400
No WESP, #/m <sup>3</sup>	1e4	2.66e8	2.44e9	4.48e7	7.06e8	2.3e9	9.92e9	4.24e9	3.95e8	9.09e5	3.51e4	1.01e7	2.93e6
With WESP, #/m <sup>3</sup>	4.65e11	7.34e11	1.69e11	2.33e10	1.03e10	1.86e9	1.22e9	4.3e8	2.07e8	4.34e7	3.42e7	5.68e6	4.2e6

Classes 1 and 2 are merged into class 3, and classes 10-13 are disregarded



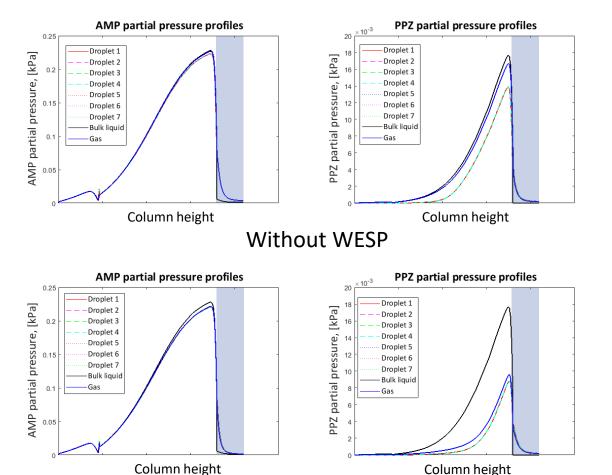
Typical concentration profiles for AMP and PPZ. Droplet initial diameter 87 nm

- Intercooling causes rapid changes in AMP and PPZ concentrations because of water condensation and evaporation
- Dry bed has a strong effect on the droplet AMP concentration but not on the PPZ concentration
- Results without WESP are very similar

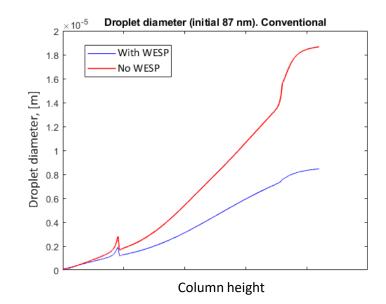




#### Partial pressure profiles for AMP and PPZ. Conventional case



With WESP



Particle number concentration is 20x larger with WESP. Giving:

- Slightly more AMP gas phase depletion with WESP
- Much more PPZ gas phase depletion with WESP
- Less particle growth with WESP and smaller particles leaving the water wash
- Dry bed case shows similar trends as the conventional case



#### Comparison of emissions in mg/Nm<sup>3</sup>

	Conventional no WESP			ntional ESP	Dry no V	bed VESP	Dry bed WESP	
	AMP PPZ		AMP	PPZ	AMP	PPZ	AMP	PPZ
Experimental	26-28	8-9	29-30	9-10	~0	1.5	~0	2.3
Model, aerosol	~0	~0	1	5.7	~0	~0	0.1	3.3
Model, gas phase	45.5	7.2	50.6	5.4	1.0	0.7	2.1	1.4

• Experimental emissions are total, whereas model emissions are aerosol and gas separately



### Conclusions



- Need of sufficient testing time to reach steady-state (especially for the water-wash section)
- The AMP/PPZ system is complex, and it seems that small particles(<20nm) grow more than in MEA. Additionally, gas phase emissions seem over-predicted by the model
- Only initial rate kinetic data are available, making the kinetic model uncertain. However, the model does behave well.
- The reason for improved operation with a dry bed seems to be that it is not dry, but constitutes an extra wash section
- Using WESP leads to higher particle numbers, leading to more gas phase amine depletion and less particle growth
- Several emission mitigation configurations are available to control volatile and aerosol-based emissions and are holistically evaluated in SCOPE





#### Acknowledgements

This project is funded through the ACT programme (Accelerating CCS Technologies), ACT 3 Project No 327341. Financial contributions made by the Research Council of Norway (RCN), Rijksdienst voor Ondernemend Nederland (RVO), Department for Business, Energy & Industrial Strategy UK (BEIS), Forschungszentrum Jülich GmbH, Projektträger Jülich (FZJ/PtJ) Germany, Department of Energy (DoE) USA and Department of Science and Technology (DST) India are gratefully acknowledged.

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Please join the side-event to the TCCS-12 conference: The fourth SCOPE Stakeholder, Policy, Research and Industry NeTwork (SPRINT) event "How to address, interact and act on the main knowledge gaps related to emissions", Thursday, 22 June 2023, 09:00 - 15:00, free of charge, online access via registration at WWW.Scope-act.org/events



